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Optimal Scheduling of Fuel-Minimal Approach Trajectories

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- 1. Introduction
- 2. Aircraft Simulation Model
- 3. Multi-Aircraft Optimization Problem
- 4. Results
- 5. Summary & Outlook



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Introduction

Computation of fuel minimal and noise minimal approach trajectories:

So far:

- ⇒ Optimization of **stand-alone** approach trajectories
- ⇒ Limitations due to other aircraft in the vicinity of an airport are not taken into account
- ⇒ Optimization results can not be put into practice due to the limitations arising from the remaining air traffic and the daily airport business

Here:

- ⇒ Simultaneous optimization of the approach trajectories of multiple aircraft present in the vicinity of an airport
- ⇒ Landing sequence is not pre-determined and has to be found by the optimization procedure
- ⇒ More realistic results.

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Point-Mass Simulation Model:

Position Equations of Motion (NED-Frame):

$$\begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix}_{O}^{E} = \begin{pmatrix} V_{K}^{G} \cdot \cos \chi_{K}^{G} \cdot \cos \gamma_{K}^{G} \\ V_{K}^{G} \cdot \sin \chi_{K}^{G} \cdot \cos \gamma_{K}^{G} \\ -V_{K}^{G} \cdot \sin \gamma_{K}^{G} \end{pmatrix}_{O}$$

Translation Equations of Motion:

$$\begin{pmatrix} \dot{V}_{K}^{G} \\ \dot{\chi}_{K}^{G} \\ \dot{\gamma}_{K}^{G} \end{pmatrix}_{K}^{EO} = \begin{pmatrix} 1 \\ \frac{1}{V_{K}^{G} \cdot \cos \gamma_{K}^{G}} \\ -\frac{1}{V_{K}^{G}} \end{pmatrix}_{K} \begin{pmatrix} \frac{1}{m} \left(\sum \bar{\mathbf{F}}^{G} \right)_{K} \right)$$



Total sum of external forces:

$$\left(\sum \vec{\mathbf{F}}^{G}\right)_{K} = \left(\vec{\mathbf{F}}_{A}^{G}\right)_{K} + \left(\vec{\mathbf{F}}_{P}^{G}\right)_{K} + \mathbf{M}_{KO} \cdot \left(\vec{\mathbf{F}}_{G}^{G}\right)_{O}$$

Thrust modeling:

$$T = \delta_T \cdot T_{\text{max}}$$

$$T_{\text{max}} = T_{\text{max},ISA} \cdot \left(1 - C_{Tc5} \cdot \Delta T_{ISA,eff}\right)$$

$$T_{\text{max},ISA} = C_{Tc1} \cdot \left(1 - \frac{h}{C_{Tc2}} + C_{Tc3} \cdot (h)^2\right)$$

$$\Delta T_{ISA,eff} = \Delta T_{ISA} - C_{Tc4}$$

Aerodynamic coefficients:

$$C_D = C_{D0} + C_{D2} \cdot C_L^2$$

$$C_L = C_{L0} + C_{L\alpha} \cdot \alpha_{A,CMD}$$

Aerodynamic Forces:

$$D = \overline{q} \cdot S \cdot C_D = \overline{q} \cdot S \cdot \left(C_{D0} + C_{D2} \cdot C_L^2 \right)$$

$$Q = \overline{q} \cdot S \cdot C_Q = \overline{q} \cdot S \cdot C_{Q\beta} \cdot \beta_A = 0$$

$$L = \overline{q} \cdot S \cdot C_L = \overline{q} \cdot S \cdot (C_{L0} + C_{L\alpha} \cdot \alpha_A)$$

Dynamic pressure:

$$\overline{q} = 0.5 \cdot \rho \cdot V_A^2$$

Force vector:

$$\left(\vec{\mathbf{F}}^{G}\right)_{A} = \left(\vec{\mathbf{F}}_{A}^{G}\right)_{A} + \left(\vec{\mathbf{F}}_{P}^{G}\right)_{A} = \begin{pmatrix} -D\\0\\-L \end{pmatrix}_{A} + \begin{pmatrix} T\\0\\0\\A \end{pmatrix} = \begin{pmatrix} T-D\\0\\-L \end{pmatrix}_{A}$$

Noise model:

Sound pressure level:

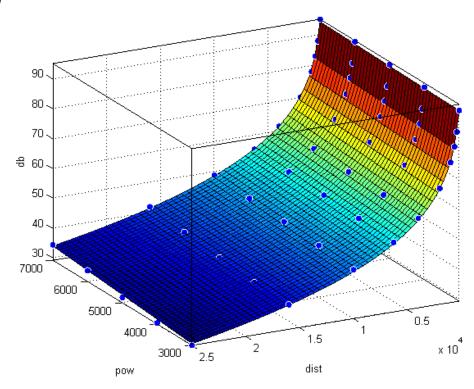
$$L_A(T,r) = a \cdot T + b \cdot \lg(r) + c \cdot \lg(r)^2 + d$$

Sound exposure level:

$$L_{AE} = 10 \lg \left(\frac{1}{t_0} \int_{t_1}^{t_2} 10^{L_A(t)/10} dt \right)$$

Number of Awakenings:

$$n_{AW} = \sum_{i} 0.0087 \cdot (L_{AE,i} - 30)^{1.79} p_{i}$$



Atmospheric model (DIN ISO 2533):

$$H_{G} = \frac{r_{E} \cdot h}{r_{E} + h}$$

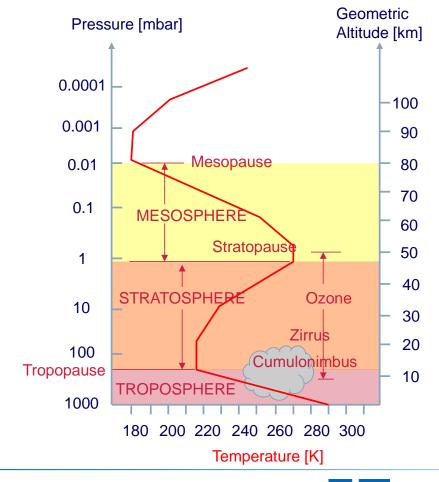
$$\rho = \rho_{S} \left[1 + \frac{\gamma_{Tr}}{T_{S}} \cdot H_{G} \right]^{\left(-\frac{g_{S}}{R \cdot \gamma_{Tr}} - 1 \right)}$$

$$p = p_{S} \left[1 + \frac{\gamma_{Tr}}{T_{S}} \cdot H_{G} \right]^{\left(-\frac{g_{S}}{R \cdot \gamma_{Tr}} \right)}$$

Fuel consumption:

$$\begin{split} \dot{m}_{\textit{fuel},\textit{idle}} &= C_{f3} \cdot \left(1 - \frac{h}{C_{f4}}\right) \\ \dot{m}_{\textit{fuel},\text{max}} &= C_{f1} \cdot \left(1 + \frac{V_A}{C_{f2}}\right) \cdot T_{\text{max}} \end{split}$$

$$\dot{m}_{fuel} = \dot{m}_{fuel,idle} + \delta_T \cdot \left(\dot{m}_{fuel,max} - \dot{m}_{fuel,idle} \right)$$



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Determine the optimal control histories

$$\mathbf{u}_{i,opt}(t_i) \in \mathbf{P}^m$$

and the corresponding optimal state trajectories

$$\mathbf{x}_{i,opt}(t_i) \in \mathbf{P}^n$$

that **minimize** the Bolza cost functional

$$J = \sum_{i=1}^{N} \left[e_i \left(\mathbf{x}_i \left(t_{f,i} \right), t_{f,i} \right) + \int_{t_{0,i}}^{t_{f,i}} L_i \left(\mathbf{x}_i \left(t_i \right), \mathbf{u}_i \left(t_i \right), t_i \right) dt_i \right]$$

subject to

- ⇒ the state dynamics
- ⇒ the initial boundary conditions
- ⇒ the final boundary conditions
- ⇒ the interior point conditions
- ⇒ the equality constraints
- ⇒ and the inequality constraints

$$\dot{\mathbf{x}}_{i}(t_{i}) = \mathbf{f}_{i}(\mathbf{x}_{i}(t_{i}), \mathbf{u}_{i}(t_{i}), t_{i})$$

$$\psi_{0,i}(\mathbf{x}_i(t_{0,i}),t_{0,i}) = \mathbf{0} \qquad \psi_{0,i} \in \mathbf{P}^{q_i}$$

$$\psi_{f,i}(\mathbf{x}_i(t_{f,i}),t_{f,i}) = \mathbf{0} \qquad \psi_{f,i} \in \mathbf{P}^{p_i}$$

$$\mathbf{r}_{i}(\mathbf{x}(t_{i}),t_{i})=\mathbf{0} \qquad \mathbf{r}_{i} \in \mathbf{P}^{k_{i}}$$

$$\mathbf{C}_{eq,i}(\mathbf{x}_i(t_i),\mathbf{u}_i(t_i),t_i) = \mathbf{0}$$
 $\mathbf{C}_{eq,i} \in \mathbf{P}^{r_i}$

$$\mathbf{C}_{ineq,i}(\mathbf{x}_i(t_i),\mathbf{u}_i(t_i),t_i) \leq \mathbf{0}$$
 $\mathbf{C}_{ineq,i} \in \mathbf{P}^{s_i}$

i = 1,..., N

Initial boundary conditions:

⇒ Defined by the entry position into the considered air space

Final boundary conditions:

- ⇒ Assure that the aircraft are finally located on the ILS glide path
- \Rightarrow Final approach fix: located at the origin of the Local Fixed Frame N at an altitude of h_{FAF}
- \Rightarrow ILS glide path: directed parallel to the x-axis of the Local Fixed Frame N, into the direction of the positive x-axis

Final boundary conditions:

$$\Rightarrow$$
 Northward position: $x(t_f) \ge x_{FAF} + \Delta x$

$$\Rightarrow$$
 Eastward position: $y(t_f) = y_{FAF}$

$$\Rightarrow$$
 Altitude: $h(t_f) = h_{FAF} + \tan(-\gamma_{K,ILS}) \cdot x(t_f)$

$$\Rightarrow$$
 Glide-path angle: $\gamma_K(t_f) = \gamma_{K,ILS}$

$$\Rightarrow$$
 Heading angle: $\chi_K(t_f) = \chi_{K,ILS}$

$$\Rightarrow$$
 Kinematic velocity: $V_K(t_f) = V_{K,ILS}$

Inequality path constraints:

$$\Rightarrow$$
 Load factor: $n_{Z,LB} = 0.85 \le n_Z(t) \le 1.15 = n_{Z,UB}$

$$\Rightarrow$$
 Kinematic velocity: $V_{K,LB} = 200 \frac{km}{h} \le V_K(t) \le 1000 \frac{km}{h} = V_{K,UB}$

$$\Rightarrow$$
 Angle of attack: $\alpha_{A,CMD,LB} = -5.73^{\circ} \le \alpha_{A,CMD} \le 20.05^{\circ} = \alpha_{A,CMD,UB}$

$$\Rightarrow$$
 Bank angle: $\mu_{K,CMD,LB} = -45^{\circ} \le \mu_{K,CMD} \le 45^{\circ} = \mu_{K,CMD,UB}$

$$\Rightarrow$$
 Thrust lever: $\delta_{T,CMD,LB} = 0.0 \le \delta_{T,CMD} \le 1.0 = \delta_{T,CMD,UB}$

$$\Rightarrow$$
 Eastward position: $y_{LB}(t) \le y(t) \le y_{UB}(t)$

$$\Rightarrow$$
 Altitude: $h_{LB}(t) \le h(t) \le h_{UB}(t)$

$$\Rightarrow$$
 Aircraft distance: $d_{ii}(t) - d_{\min} \ge 0$

Inequality path constraints:

- ⇒ Path constraints are formulated such that the aircraft have to follow the ILS glide path once the FAF has been passed
- ⇒ Eastward position:

$$y_{LB}(t) = 0.5 \cdot [1 - \tanh(a \cdot x(t))] \cdot y_{LB} - 100.0$$

$$y_{UB}(t) = 0.5 \cdot [1 - \tanh(a \cdot x(t))] \cdot y_{UB} + 100.0$$

⇒ Altitude:

$$h_{LB}(t) = 0.5 \cdot [1 - \tanh(a \cdot x(t))] \cdot h_{LB} + (h_{FAF} - 100.0) + \tan(-\gamma_{ILS}) \cdot x(t)$$

$$h_{UB}(t) = 0.5 \cdot [1 - \tanh(a \cdot x(t))] \cdot h_{UB} + (h_{FAF} + 100.0) + \tan(-\gamma_{ILS}) \cdot x(t)$$

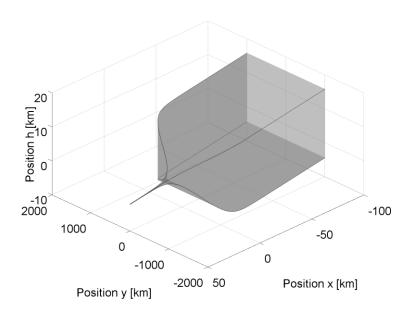
⇒ Kinematic velocity:

$$V_{K,LB}(t) = 0.5 \cdot [1 - \tanh(a \cdot x(t))] \cdot (V_{K,LB} - V_{K,LLS} + 10.0) + (V_{K,LLS} - 10.0)$$

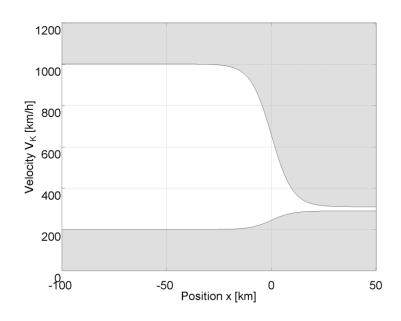
$$V_{K,UB}(t) = 0.5 \cdot \left[1 - \tanh(a \cdot x(t))\right] \cdot \left(V_{K,UB} - V_{K,ILS} - 10.0\right) + \left(V_{K,ILS} + 10.0\right)$$

Inequality path constraints:

⇒ Path constraints are formulated such that the aircraft have to follow the ILS glide path once the FAF has been passed



Permitted airspace



Path constraints w.r.t. kinematic velocity V_K

Inequality path constraints:

⇒ A certain separation distance between the aircraft has to be maintained

Aircraft distances:

$$d_{ij}(t) = \sqrt{\left[x_i(t) - x_j(t)\right]^2 + \left[y_i(t) - y_j(t)\right]^2 + \left[z_i(t) - z_j(t)\right]^2}, \quad i = 1, ..., N, j = i + 1, ..., N$$

Normalization of flight times w.r.t. final flight times:

$$\tau_i = \frac{t_i}{t_{f,i}}, i = 1, ..., N$$

Introduction of **one** single parameter for all flight times:

$$t_f = t_{f,1} = t_{f,2} = \dots = t_{f,N}$$

- ⇒ The time elapsed is the **same** for all aircraft
- ⇔ Constraints w.r.t. the minimum distances can be checked directly (because of the direct correlation of the time elapsed)

Cost function:

Fuel-minimal approaches: maximize aircraft masses at the final times

$$J = -\sum_{i=1}^{N} m_i \left(t_{f,i} \right)$$

Noise-minimal approaches: minimize maximum sound pressure level or number of awakenings

Integral cost functions:

- ⇒ The same flight time for all aircraft is enforced
- ⇒ Aircraft are located on different positions on the ILS glide path (i.e. they have covered different distances)
 - ⇒ Equal weighting of the aircraft has to be achieved

Portion of the integral cost function originating from flight along ILS glide path is not incorporated into the integral cost function:

$$\dot{m}_{fuel,eff}(t) = \dot{m}_{fuel}(t) \cdot 0.5 \cdot \left[1 - \tanh\left(a \cdot \left[x(t) - \Delta x_{fuel}\right]\right)\right]$$

Full-Discretization Method – Forward (explicit) Euler:

⇒ Time discretization (e.g. equidistant):

$$\tau_i = t_0 + (i-1) \cdot h, \quad i = 1, ..., N, \quad h = \frac{t_f - t_0}{N-1}$$

⇒ Discretization of controls and states at time discretization points:

$$\mathbf{x}_i, \mathbf{u}_i, \quad i = 1, ..., N$$

⇒ Approximation of differential equations:

$$\mathbf{x}_{i+1} = \mathbf{x}_i + h \cdot \mathbf{f}(\mathbf{x}_i, \mathbf{u}_i, \mathbf{p}), \qquad i = 1, ..., N-1$$

⇒ Additional equality constraints:

$$\mathbf{x}_{i+1} - \mathbf{x}_i - h \cdot \mathbf{f}(\mathbf{x}_i, \mathbf{u}_i, \mathbf{p}) = \mathbf{0}, \quad i = 1, ..., N-1$$

Discretized Optimal Control Problem (Euler):

Determine the optimal parameter vector $\mathbf{z} = [\mathbf{x}, \mathbf{u}]^T$

that minimizes the cost function $J(\mathbf{z})$

subject to

⇒ the inequality constraints

 $C_{ineq}(x(z),z) \leq 0$

⇒ and the equality constraints

$$\mathbf{C} = \begin{pmatrix} \mathbf{\psi}_{0}(\mathbf{x}(\mathbf{z}), \mathbf{z}) \\ \mathbf{C}_{eq}(\mathbf{x}(\mathbf{z}), \mathbf{z}) \\ \mathbf{x}_{i+1} - \mathbf{x}_{i} - h \cdot \mathbf{f}(\mathbf{x}_{i}, \mathbf{u}_{i}) \\ \mathbf{r}(\mathbf{x}(\mathbf{z}), \mathbf{z}) \\ \mathbf{\psi}_{f}(\mathbf{x}(\mathbf{z}), \mathbf{z}) \end{pmatrix} = \mathbf{0}$$

⇒ **SNOPT** (sequential quadratic programming SQP)

Solution Strategy:

- (1) Optimization without distance path constraints
- (2) Simultaneous optimization with distance path constraints, using previous results as initial guess
 - ⇒ Distance path constraints fulfilled by initial guess:
 Initial guess = Optimal solution of constrained problem
 - ⇒ Distance path constraints **not** fulfilled by initial guess: Separation of aircraft until path constraints are met

Assumptions:

- ⇒ Optimal solution of unconstrained problem = Excellent initial guess of constrained problem
- ⇒ Cost function of a specific optimization problem is always less than or equal to the cost function of the same trajectory optimization problem with additional constraints

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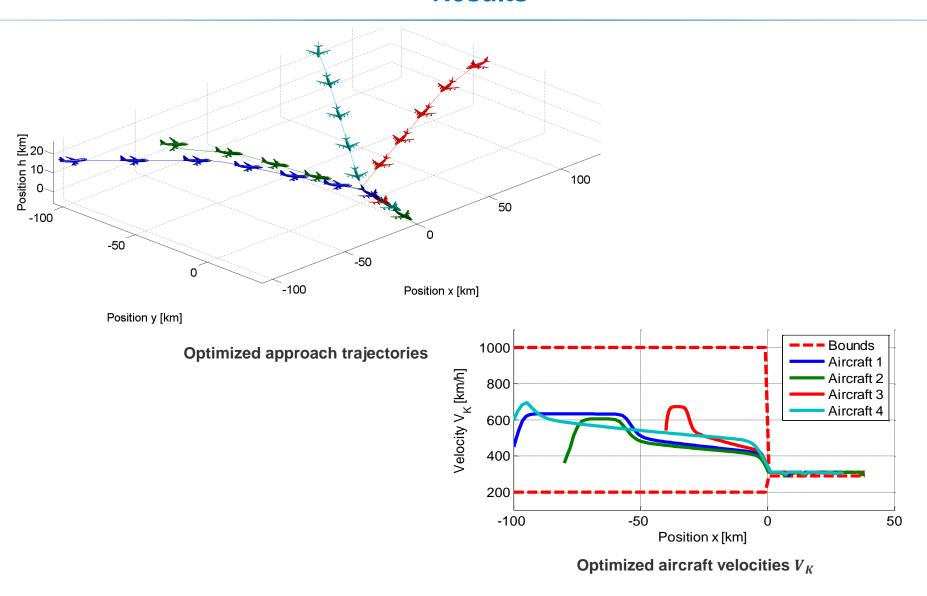
Results

Generic scenario:

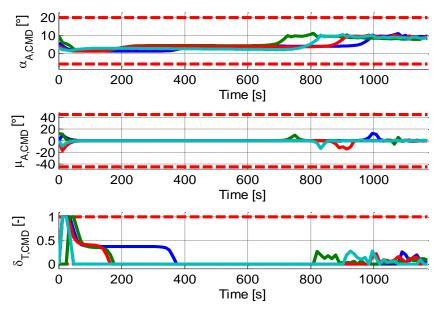
- The optimal landing sequence and the optimal approach trajectories for **four** aircraft are sought
- ⇒ Initial conditions:

AC No.	1	2	3	4
$x_{i,0}$	-100000 m	-80000 m	-40000 m	-100000 m
$y_{i,0}$	100000 m	50000 m	-120000 m	-70000 m
$h_{i,0}$	4000 m	4000 m	5000 m	6000 m
$\chi_{K,i,0}$	-60.0°	-45.0°	95.0°	45.0°
$\gamma_{K,i,0}$	0.0°	0.0°	0.0°	0.0°
$V_{K,i,0}$	450.0 km/h	360.0 km/h	540.0 km/h	600.0 km/h

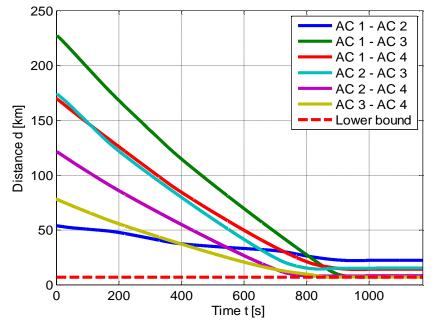
Results



Results



Optimized time histories of aircraft controls



Distances between aircraft

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Summary

- ⇒ The approach trajectories of multiple aircraft in the vicinity of an airport have been optimized simultaneously
- ⇒ Path constraints have been introduced so that the aircraft are finally located on the ILS glide path and keep a certain separation distance.
- ⇒ The optimal landing sequence is determined by the optimization procedure

Outlook

- ⇒ Utilization of splines to describe the centerlines of the allowed flight path corridors for the involved aircraft
- Introduction of path constraints w.r.t. the maximum lateral and horizontal deviation from the centerlines
- More sophisticated distance path constraints between aircraft

Thank you very much for your attention!